$n^{2} + n - 6 = 0$ (n + 3) (n - 2) = 0, n = 2

Overall diameter of the conductor, $D = (1 + 2n) d = (1 + 4) \times 29 = 14.5$ mm

The *equivalent cross-section* of a stranded conductor is the area of cross-section of a solid conductor of the same material and length as the stranded conductor and having the same resistance at the same temperature. For convenience, the conductors are identified by their code names assigned by the manufacturers. Usually names of some animals, birds or flowers are used.

3.2 1 YPES OF CONDUCTORS

Hard-drawn copper, hard-drawn aluminium, and steel-cored aluminium conductors are most commonly used. In addition to these, various other materials are used for making conductors but their use is limited. Some of the important types of conductors are given in the discussion as follows.

3.2.1 Hard-Drawn Copper Conductors

Copper for overhead lines is hard-drawn to give a relatively high tensile strength. It has a high electrical conductivity, long life, and high scrap value. Other properties of hard-drawn copper are given in Table 3.1 along with the properties of hard-drawn aluminium. Copper conductor is most suitable for distribution work where spans are short and tappings are more.

Table 3.1. Electrical and Mechanical Characteristics of Hard-Diawn Aluminium and Copper Wires

	Hard-d-awn alumini-m	Hard-drawn copper
Conductivity at 20°C IACS*	61	97.4
Resistivity at 20°C (microhm-cm)	2.8264	1.774
Resistivity temperature coefficient (microhm-cm °C)	0.0115	0.00681
Constant mass temperature coefficient of resistance per °C at 20°C	0.00403	0.00381
Coefficient of linear expansion per °C	2.3×10^{-5}	1.7×10^{-5}
Density at 20°C (gm/cm ³)	2.703	8.89
Ultimate tensile strength (kgf/mm ²)	16.21	35-47
Final modulus of elasticity (kgf/mm ²)	7000 average	12700 average

* International Annealed Copper Standard

3.2.2 Cadmium Copper Conductor

The tensile strength of copper is increased by approximately 50 per cent by adding about 0.7 to 1.0 per cent cadmium to it. The conductivity is, however, reduced by about 15 to 17 per

Combination of Eqs. (4.11.1) and (4.11.2) gives

$$g_x = \frac{V}{x \ln (R/r)}$$
 V/m ...(4.11.3)

The maximum stress will occur at the smallest radius, i.e., for x = r. The stress is a maximum at the surface of conductor, or in other words, the inner most layer of the dielectric is subjected to a maximum stress. The maximum stress is given by

$$g_{\max} = \frac{V}{r \ln \frac{R}{r}} \quad V/m \qquad \dots (4.11.4)$$

When x = R, the stress will be a minimum which indicates that stress has a minimum value at the sheath. The minimum value is given by

$$g_{\min} = \frac{V}{R \ln \frac{R}{r}} \quad \text{V/m} \qquad \dots (4.11.5)$$

Also,
$$\frac{g_{\text{max}}}{g_{\text{min}}} = \frac{\kappa}{r}$$
 ...(4.11.6)

The electric stress in a belted cable cannot be calculated accurately due to non-uniformity of the dielectric and the distortion in the electrostatic field.

The present day tendency is to design high voltage cables on the basis of a fixed maximum value of operating stress. The stress is usually expressed in kilovolts per millimetre. Eq. (4.11.4) is then utilized to determine the thickness of insulation necessary for a given diameter of conductor. It is clear from Eq. (4.11.4) that greater the value of permissible stress the lesser will be the insulation thickness. It is desirable to choose a higher value of operating stress in order to have a reduced thickness of insulation and, therefore, a reduced size of cable. Since a smaller cable size affords more economy, there is a tendency to increase the operating stresses to their highest values without the failure to cable either under actual operating conditions or during its approval specified tests.

Considerably improvements have been made in developing high strength paper, conductor screening and manufacturing techniques to achieve the objective of operating the cable at maximum stress levels.

Most Economical Size of Cable

Maximum potential gradient,
$$g_{\text{max}} = \frac{V}{r \ln \frac{R}{r}}$$

If V and R are constant and r is made variable the expression for g_{max} has a minimum value when $r \ln (R/r)$ is a maximum. This occurs when

$$\frac{d}{dr} \left(r \ln \frac{R}{r} \right) = 0 ; \qquad \frac{d}{dr} \left(r \ln R - r \ln r \right) = 0$$

$$\ln R - r \cdot \frac{1}{r} - \ln r = 0 ; \qquad \ln \frac{R}{r} = 1 = \ln e ; \qquad \frac{R}{r} = e = 2.718$$

4. Larger and stronger steel pipes are needed for bigger sizes of conductor. The pipes have to withstand gas pressures of the order of 1.725×10^6 N/m².

The pipe may as well be filled with oil, which although more costly than nitrogen gas, permits higher dielectric operating stresses than the cheaper gas filling.

4.28 COMPRESSED GAS INSULATED CABLES (GIC)

In a compressed gas insulted cable, high pressure sulphur hexafluoride (SF_6) gas fills the small spaces in oilimpregnated paper insulation and suppresses the ionization.

The conductors in gas insulated cables consist of hollow aluminium tubes rather than solid rods in order to have greater rigidity, lower electrical surface stress, and lower ac-dc resistance ratio. They are subject to severe mechanical, thermal and electrical stresses. It is, therefore, necessary to hold these conductors in position by spacers. Three types of spacers are used in rigid gas insulted cables. They are (a) disc type, (b) cone type, and (c) post type as shown in Fig. 4.27.

The spacers are made from epoxy resin insulating material. There are two possible configurations :

(a) Isolated phase GIC

(b) Single enclosure type three-phase GIC

In an *isolated phase GIC*, the three phases are enclosed in *separate enclosures*, filled with SF₆ gas at a pressure of 2 to 4 atmospheres $(2 \times 10^5 \text{ to } 4 \times 10^5 \text{ N/m}^2)$ as shown in Fig. 4.28 (a). When all the three phases are put into the same enclosure (pipe or sheath), the configuration is called *single-enclosure three-phase GIC* [Fig. 4.28 (b)]. The enclosure is filled with SF₆ gas at a pressure of 2 to 4 atmospheres. The enclosure is made from an aluminium alloy for greater mechanical strength.

The choice between the GIC configurations is made on space and economic considerations. An isolated phase system requires (a) larger quantity of aluminium for enclosure pipes and (b) wider trenches. The rigid three-phase GIC system provide economies in metal consumption and trench width, but its current-carrying capacity is less than an isolated GIC system.

Most of the gas cables presently in use consist of three separate coaxial lines assembled from rigid pipes of aluminium alloy.

EHV/UHV lines insulated with sulphur hexafluoride (SF₆) gas are being used extensively for voltages above 132 kV upto 1200 kV.

GIC systems are very popular for short lengths, river crossings, and highway crossings, etc.



Fig. 4.27. Spacers used in rigid isolated phase gas insulated cables. (a) Disc, (b) Cone, (c) Post.

Solution

Let C represent the self capacitance of each unit. The capacitances of the link pins to earth and to the line will, therefore, be 0.2C and 0.1C respectively. The capacitances, voltages and currents are shown in Fig. 5.16.

(a) We have

....

Also,

and

$$I_{1} = v_{1} (j \omega C), I_{a} = v_{1} (j \omega) (0.2C)$$

$$i_{1} = (V - v_{1}) j \omega (0.1C)$$

$$I_{2} = I_{1} + I_{a} - i_{1}$$

$$= v_{1} j \omega C + 0.2v_{1} j \omega C - 0.1 (V - v_{1}) j \omega C$$

$$= j \omega C (1.3v_{1} - 0.1V)$$

$$v_{2} = \frac{I_{2}}{j \omega C} = 1.3v_{1} - 0.1V$$

$$I_{b} = (v_{1} + v_{2}) \times 0.2 j \omega C = (v_{1} + 1.3v_{1} - 0.1V) \times 0.2j \omega C = j \omega C (0.46v_{1} - 0.02V)$$

$$i_{2} = v_{3} \times 0.1j \omega C$$

$$I_{3} = I_{2} + I_{b} - i_{2}$$

$$= j\omega C (1.3v_{1} - 0.1V) + j\omega C (0.46v_{1} - 0.02V) - 0.1 j\omega C v_{3}$$

$$= j\omega C (1.76v_{1} - 0.12V - 0.1v_{2})$$

$$v_{3} = \frac{I_{3}}{j\omega C} = 1.76v_{1} - 0.12V - 0.1v_{3}$$

$$v_{3} = \frac{I.76v_{1}}{1.1} - \frac{0.12V}{1.1} = 1.6v_{1} - 0.109V$$

$$v_{1} + v_{2} + v_{3} = V$$

$$v_{1} + 1.3v_{1} - 0.1V + 1.6v_{1} - 0.109V = V$$

$$3.9v_{1} = 1.209V, \quad v_{1} = \frac{1.209}{3.9} V = 0.31V$$

$$v_{2} = 1.3v_{1} - 0.1V = 1.3 \times 0.31V - 0.1V = 0.303V$$

$$v_{3} = 1.6v_{1} - 0.109V = 1.6 \times 0.31V - 0.109V = 0.387V$$
String efficiency $= \frac{V}{3v_{3}} = \frac{V}{3 \times 0.387V} = 0.8613$ pu

(b) With the grading ring

The capacitance of the lower link pin now becomes 0.35C instead of 0.1C. Therefore,

$$i_2 = v_3 \times 0.35 \, j\omega C$$

 $I_3 = I_2 + I_b - i_2 = j\omega C \, (1.76v_1 - 0.12V - 0.35v_3)$



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Example 1.5 The load-duration curve for a system is shown in Fig. 1.2. Determine the load factor.

Solution

From the load-duration curve, the actual energy consumed $= 15 \times 8 + 10 \times 8 + 5 \times 8 = 240$ MWh

240

Average load =
$$\frac{240}{24}$$
 = 10 MW
Maximum demand = 15 MW
Load factor = $\frac{\text{average load}}{\text{maximum demand}}$ = $\frac{10}{15}$ = 0.666



Example 1.6 The yearly load duration curve of a power plant is a straight line. The maximum load is 500 MW and the minimum load is 400 MW. The capacity of the plant is 750 MW. Find (a) plant capacity factor, (b) load factor, (c) utilization factor, (d) reserve capacity.

Solution

Average annual load =
$$\frac{500 + 400}{2}$$
 = 450 MW
Capacity factor = $\frac{\text{average annual load}}{\text{capacity of the plant}}$ = $\frac{450}{750}$ = 0.6
Load factor = $\frac{\text{average load}}{\text{maximum demand}}$ = $\frac{450}{500}$ = 0.9
Utilization factor = $\frac{\text{maximum demand}}{\text{capacity of the plant}}$ = $\frac{500}{750}$ = 0.667

Reserve capacity = plant capacity - maximum demand = 750 - 500 = 250 MW

Example 1.7 A power system had the daily load curve given by the following table :

Time	Load in MW
12.00 night to 2 a.m.	20
2 a.m. to 8 a.m.	10
8 a.m. to 12.30 noon	50
12.30 noon to 1.00 p.m.	40
1.00 p.m. to 6 p.m.	50
6 p.m. to 12 night	70

Plot the following curves :

(a) Chronological load curve

(b) Load-duration curve